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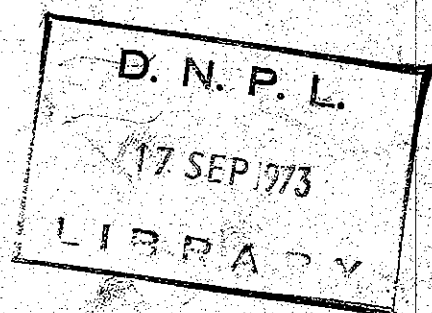
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Stability of Beam-Cavity System

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Stability of Beam-Cavity System

The stability of a Beam-Cavity System has been investigated by K. W. Robinson and a 4th order algebraic equation derived, from which the complex resonant frequencies of the system may be found.

The equation has been evaluated for the parameters of NINA with different conditions of R. F. tuning.

The equation, with a slight change in nomenclature is as follows:

$$\delta^4 + \delta^3 \cdot 2\alpha + \delta^2 \cdot \left[\Omega^2 + \alpha^2 + \alpha^2 \tan^2 \psi \right] + \delta \cdot 2\alpha \Omega^2 + \left[\alpha^2 + \alpha^2 \tan^2 \psi - \alpha^2 \frac{V_L}{V} \frac{\tan \psi}{\cos \phi} \right] \Omega^2 = 0$$

where $\Omega = \left[\frac{2\pi r^2 \alpha' V \beta \cos \phi}{E_s} \right]^{\frac{1}{2}}$ the synchronous angular frequency of the individual electrons in the synchrotron.

$\alpha = \frac{\omega_0}{2Q_L}$ the natural rate of response of the tuned circuit

$\omega_0 =$ the natural angular resonant frequency of the tuned circuit

$Q_L =$ loaded Q factor of the tuned circuit

$\psi =$ angular detuning of the tuned circuit, given by the admittance $Y = G(1+j \tan \psi)$

$f =$ RF. drive frequency

$\alpha' =$ orbit compaction factor.

$V =$ peak cavity voltage.

$V_L = I_L R \beta$

$\beta =$ transit time factor of the cavity

$E_s =$ synchronous energy of electrons in the synchrotron.

$\phi =$ Phase angle of beam current w.r.t. cavity voltage as shown in figure (2)

ΔV $\Delta \phi$ etc are assumed to be changing as $A_e e^{st}$

1. CAA-11 R. F. Acceleration II by K. W. Robinson pp 14 - 10

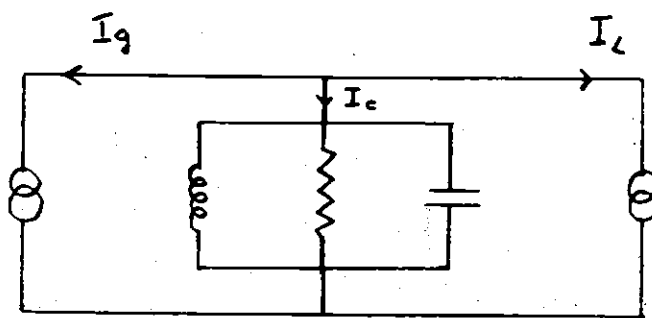


Fig (1)

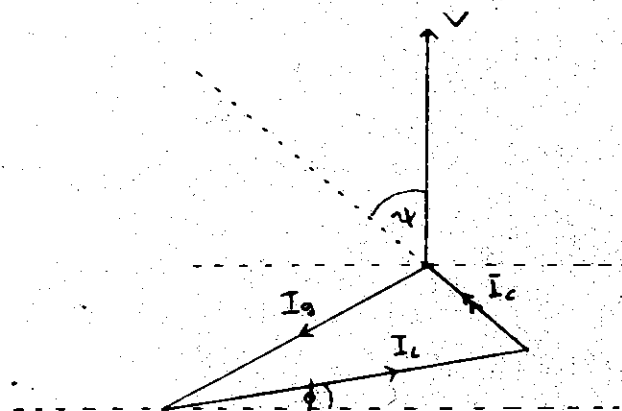


Fig (2)

I_g is the generator current

I_L is the 400 Mc/s component of the beam current. For a beam perfectly bunched at 408 Mc/s

$$I_L = 2 \bar{I}_b$$

Where $\bar{I}_b$ is the mean D. C. circulating current.

For this condition $\phi = \phi_s$ the synchronous phase angle of the individual electrons.

If P_c is the power given to the beam to keep the electrons in synchronisation

$$P_c = \bar{V} \bar{I}_b \sin \phi_s = \frac{V I_L}{2} \sin \phi$$

from "DC" beam condition

from vector diagram.

Parameters

The parameters common to all the calculations were

$$f = 400 \text{ Mc/s}$$

$$\alpha' = .0453$$

$$\beta = 2/\pi$$

$$Q_u = 4 \times 10^4 \text{ unloaded } Q$$

$$G_o = \text{cavity shunt conductance}$$

$$G_o = \text{waveguide shunt conductance as seen by the cavity.}$$

$$\text{giving } Q_L = \frac{Q_u}{6} = 6.667 \times 10^3$$

$$R = \frac{1}{G_o + G_c} = 6.667 \text{ M}\Omega$$

$$\bar{I}_b = .272 \text{ amps.}$$

The parameters common to calculations at the time of injection were

$$E_s = 4 \times 10^7 \text{ eV}$$

$$\Delta E_s = 7.4 \times 10^4 \text{ eV/turn, the increase in synchronous energy per turn.}$$

$$\epsilon = .49 = \frac{I_L}{2 \bar{I}_b}$$

The parameters common to calculation at full energy were

$$E_s = 4 \times 10^9 \text{ eV}$$

$$\Delta E_s = 1.1 \times 10^6 \text{ eV/turn}$$

$$\epsilon = 1.0$$

The variable parameters were ϕ and γ .

When γ was not specified, conditions were worked out so that the input impedance of the cavity was purely resistive, this automatically fixing γ and V .

When γ was specified this procedure was not carried out, and ϕ was kept at a fixed value, this value being such that by appropriate choice of γ the cavity could be totally matched to the waveguide.

Results.

Run (1)

Injection conditions. Reactive part of beam loading tuned out.

$$\phi = 1^\circ \text{ to } 32^\circ$$

The cavity is perfectly matched when $\phi = 22^\circ$ $\gamma = 58.85^\circ$

Graph (1A)

Real part of roots.

The real part of roots (1) and (2). For $\phi < 3^\circ$, real part of roots (1) and (2) $\approx 1.1922 \times 10^5$ changing very slowly as the beam loading increases.

The real part of roots (3) and (4) is also changing slowly.

If the real parts are designated $\alpha_1, \alpha_2, \alpha_3, \alpha_4$

$$\text{then } -2\alpha = \alpha_1 + \alpha_2 + \alpha_3 + \alpha_4 = -\frac{\omega}{Q_L}$$

$$\text{when } \alpha_1 = \alpha_2 \text{ and } \alpha_3 = \alpha_4 \text{ then } -\alpha = \alpha_1 + \alpha_3 = -1922 \cdot 10^5$$

When $\phi \approx 3^\circ$ the first 2 roots become pure real, and when $\phi \approx 27.3^\circ$ one of these roots reaches zero and then becomes positive. This

condition corresponds to the condition when $\gamma = \pi/2 - \phi$

Graph (1B) is an expanded version of (Graph A)

Graph (1C) Imaginary part of roots.

The imaginary part of roots (1) and (2) from $\phi = 0^\circ$ to $\phi = 3^\circ$ is very much less than the real part and is not significant.

The imaginary part of roots (3) and (4) $\approx \Omega$ the synchrotron oscillation frequency. Even at a very high beam loading the deviation from Ω is small.

Run (2)

Full energy conditions. Reactive part of beam loading tuned out $\phi = 1^\circ$ to 60° . The cavity is perfectly tuned when $\phi = 45^\circ$
 $\gamma = 55.7^\circ$

Graph (2A)

Real Part of roots.

Graph (2B)

Imaginary part of roots.

The imaginary part of roots (1) and (2) is again not significant.

Run (3)

Injection conditions $\phi = 22^\circ$ $\gamma = -40^\circ$ to $+80^\circ$

Graph (3A)

For cavity matched $\gamma = 55.53^\circ$

Real Part of roots.

For $\gamma < 0$ real part of roots (3) and (4) is positive and the system is unstable.

Graph (3B)

expanded version of 3A

Graph (3C)

Imaginary part of roots.

The imaginary part of roots (1) and (2) can be larger than the real part and is therefore significant.

For matched conditions at injection $\gamma = 55.53^\circ$

If γ is increased to 55° roots (1) and (2) change rapidly.

The damping is increased from 0.5×10^5 to 1.74×10^5 and the motion is oscillatory fig (3), as opposed to exponential fig (4) for the case $\gamma = 55.53^\circ$

==== roots (1) 2 (2)
 = roots (3) 3 (4)

==== roots (1) 2 (2)
 = roots (3) 3 (4)

Fig (3)

Fig (3)

The point of maximum stability is to occur with ϕ little greater than 90° .

For ϕ from 0 to 90° $\phi = 90^\circ$ $\phi = 90^\circ$

From (1)

For Part of roots, For $\phi = 90^\circ$ $\phi = 90^\circ$

The magnitudes of the roots are less than 100 to 1000 .

From (1)

For Part of roots

For ϕ if increases to 90° the magnitude of the roots ϕ and 100 becomes 100 to 1000 and 100 to 1000 . The value of ϕ for maximum stability is seen to be 90° .

Conclusions

By testing the equation for ϕ with the roots, the equation is confirmed for no roots to have positive zero parts is

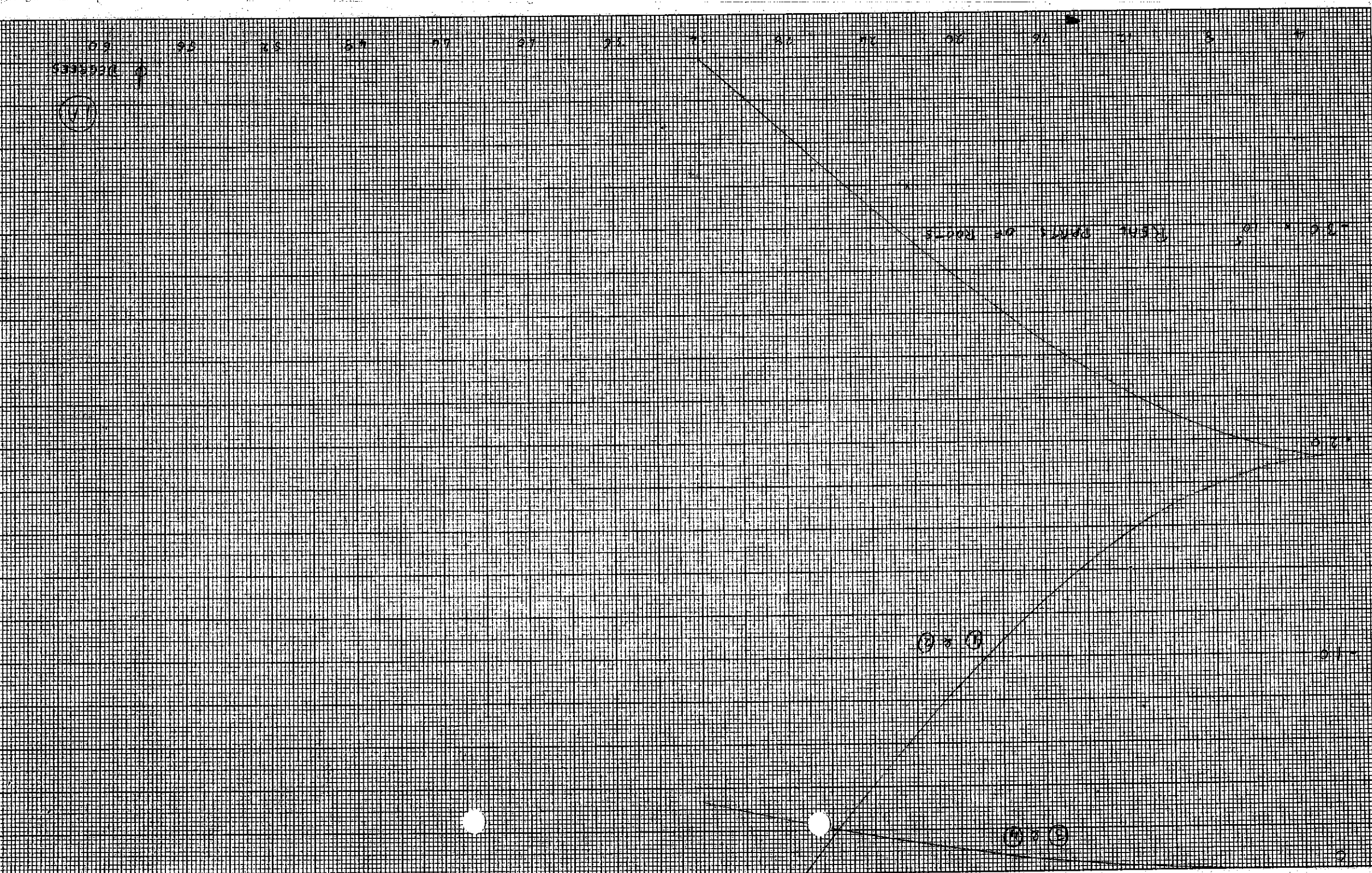
$$\phi < 90^\circ \text{ and } \phi < 90^\circ$$

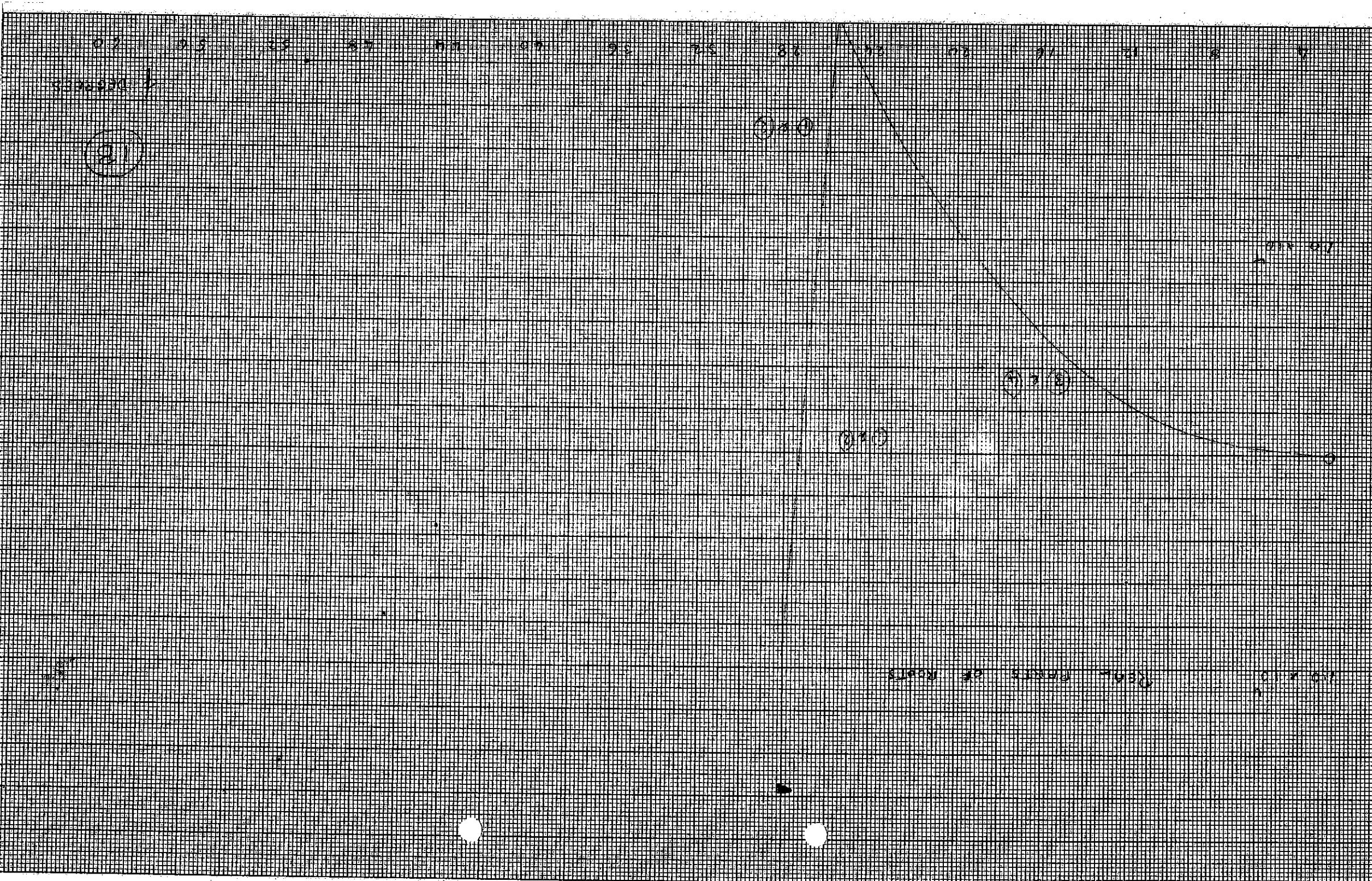
The value of the roots of the roots is less than 100 to 1000 and 100 to 1000 . The value of ϕ for maximum stability is seen to be 90° .

From (1)

The roots are calculated for ϕ from 0 to 90° and 100 to 1000 . The roots are calculated for ϕ from 0 to 90° and 100 to 1000 . The roots are calculated for ϕ from 0 to 90° and 100 to 1000 .

From (1)





0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.9 3.0 3.1 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9 4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9 5.0 5.1 5.2 5.3 5.4 5.5 5.6 5.7 5.8 5.9 6.0 6.1 6.2 6.3 6.4 6.5 6.6 6.7 6.8 6.9 7.0 7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.8 7.9 8.0 8.1 8.2 8.3 8.4 8.5 8.6 8.7 8.8 8.9 9.0 9.1 9.2 9.3 9.4 9.5 9.6 9.7 9.8 9.9 10.0

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INSTRUMENTAL CORRECTIONS

②

0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0 1.1 1.2 1.3 1.4 1.5 1.6 1.7 1.8 1.9 2.0 2.1 2.2 2.3 2.4 2.5 2.6 2.7 2.8 2.9 3.0 3.1 3.2 3.3 3.4 3.5 3.6 3.7 3.8 3.9 4.0 4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9 5.0 5.1 5.2 5.3 5.4 5.5 5.6 5.7 5.8 5.9 6.0 6.1 6.2 6.3 6.4 6.5 6.6 6.7 6.8 6.9 7.0 7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.8 7.9 8.0 8.1 8.2 8.3 8.4 8.5 8.6 8.7 8.8 8.9 9.0 9.1 9.2 9.3 9.4 9.5 9.6 9.7 9.8 9.9 10.0

02 05 25 49 77 07 08 22 42 62 82 97 121 8 7

0.0000000

0.0

Real part of roots

0.20

0.0

0.1

0.20

0.0

